

DISTRIBUTED AND OPTIMIZED SUB-SLAB VENTING (DOSSV)

Dr. L. Moorman

Radon Home Measurement and Mitigation, Inc.

Fort Collins, CO

October 30, 2023

Gary Hodgden

Midwest Radon

Olath, KS

AARST Symposium

Nashville, TN

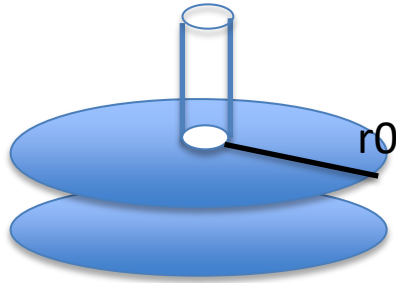
Summary of Radon Mitigation Models

- (1) Reddy-Sextro et al. model (EPA, 1992), 2 dim, air movement through soil under foundation walls.
Dynamics: Pressures and flows in plenum are vastly different close to pipe (turbulent), compared to far away (laminar).
- (2) Hantusch-Jacob model (T. McAlary, 2018), “Leaky aquafer”: 2- dim, leaks from above & leaks from below
Dynamics: Same comment as in (1).
- (3) New, DOSSV proposed for new construction allows solving a much simpler 1- dim problem, Air vacuum and flow through the aggregate bed (plenum) can be calculated for any gravel or sand with known characteristics.
Dynamics: flow is the same throughout the aggregate. (**homogeneous and isotropic**). (Viscous (laminar), or Transition regime)

Simplified Model of airflow dynamics in SSD RMS for Residences with Gravel Beds

T.A. Reddy, K.J. Gadsby, H.E. Black, III, D.T. Harrje, and R.G. Sextro,

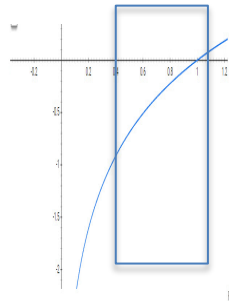
May 1992 EPA-600/R-92-090



Assumptions in the model:

- 1) Two parallel impermeable discs with radius r_0
- 2) Central extraction (or pressurization) hole
- 3) Gravel ... soil in between discs

Laminar regime: $p \sim \ln(r/r_0) + C$



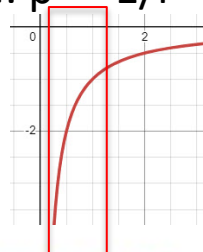
$Re \leq 1$

Larger values of r , but still

$r/r_0 < 1$

Beyond a critical circle, away from the vent pipe

Turbulent regime: $p \sim -1/r$



$Re \Rightarrow 5$ or 10

Smaller values of r , and

$r/r_0 < 1$

Within a critical circle, close to the vent pipe.

From Reddy et al.
1992

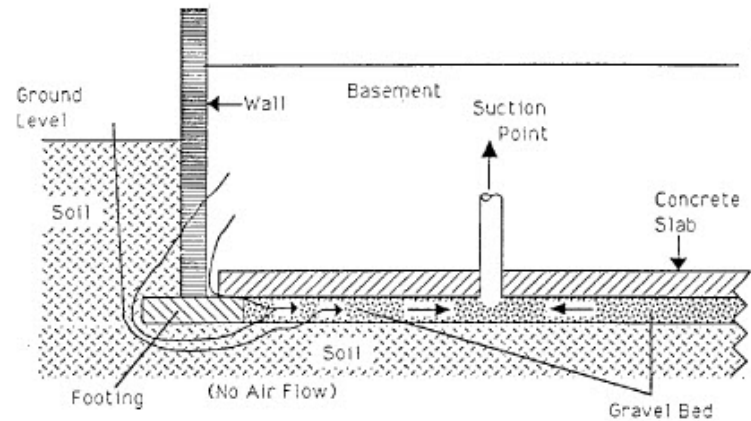


Fig. 1 Schematic of subslab air flows in a house with a gravel bed when the house is being mitigated following the subslab depressurization technique. Note that part of the air flowing through the gravel bed originates from the basement and the rest from the ambient air.

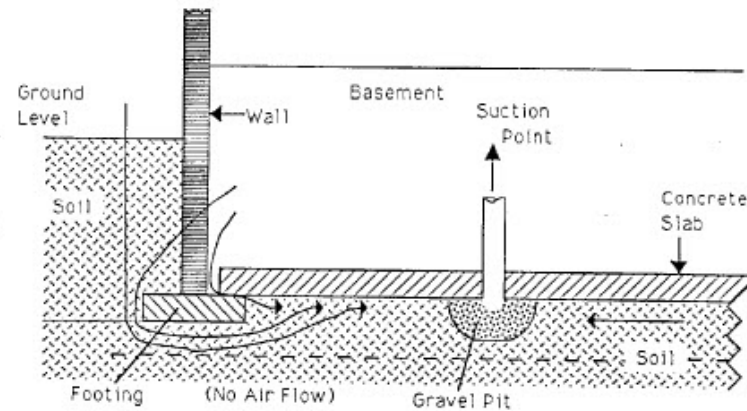
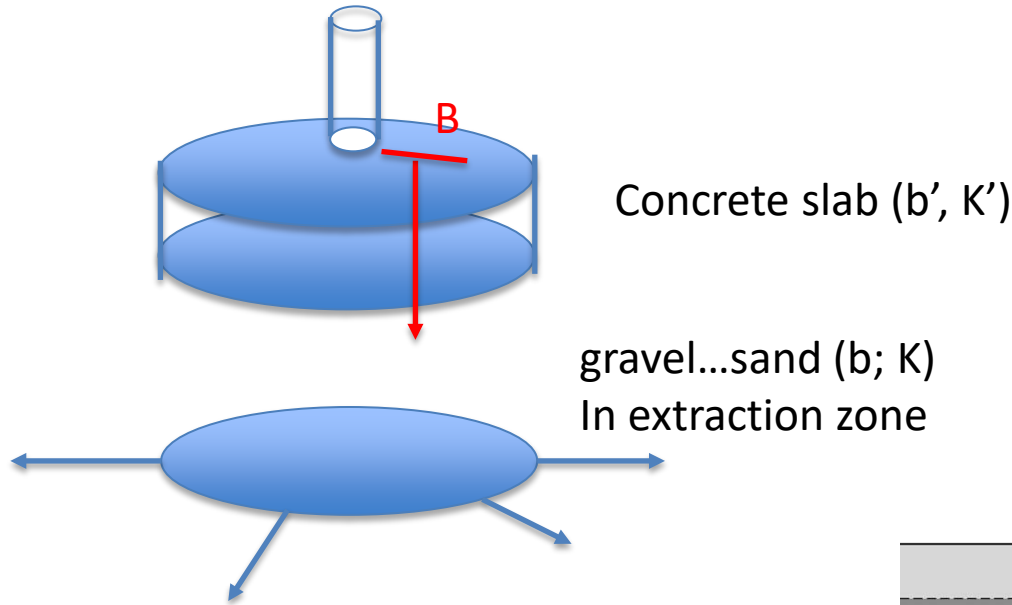


Fig. 2 Schematic of subslab air flow in a house without a gravel bed when the house is being mitigated following the subslab depressurization technique.

Summary of Research on Mitigation System design and monitoring

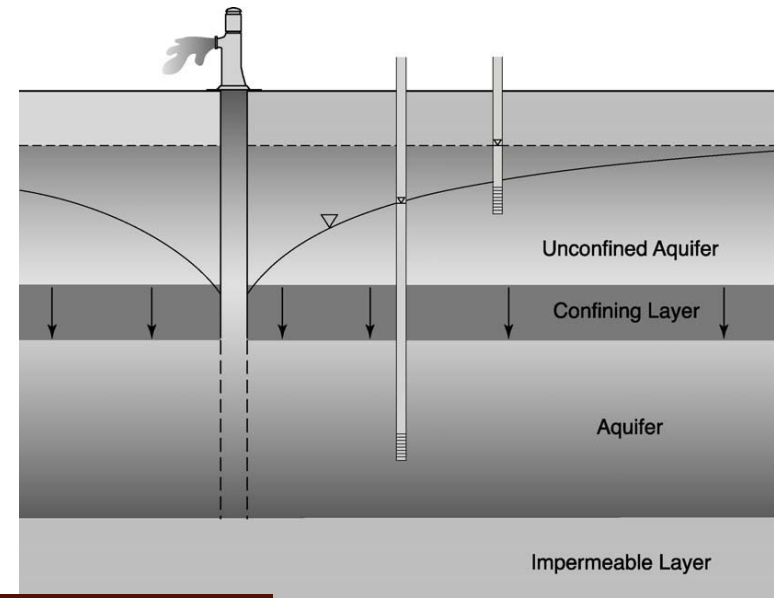
T. McAlary, W. Wertz, D. Mali, 2018, Myrtle Beach
SSD, ASD → SSV



Hantusch-Jacob Model (1955)
Laminar, and gravel, hydrodyn.
Leakance: $B [L]$ 5.5 ft...18 ft
Transmittivity $T [t]$ 54 ft²/day

$$P(\text{vacuum}) = Q_{ssv} / (2 \pi T) K_0(r/B)$$

$$\text{Velocity} = Q_{ssv} / (2 \pi b n B) K_1(r/B)$$



Fitting the functions from the model to the experimental data allows to extract unknown parameters (B, T)
(From T. McCalary, et al. 2018)

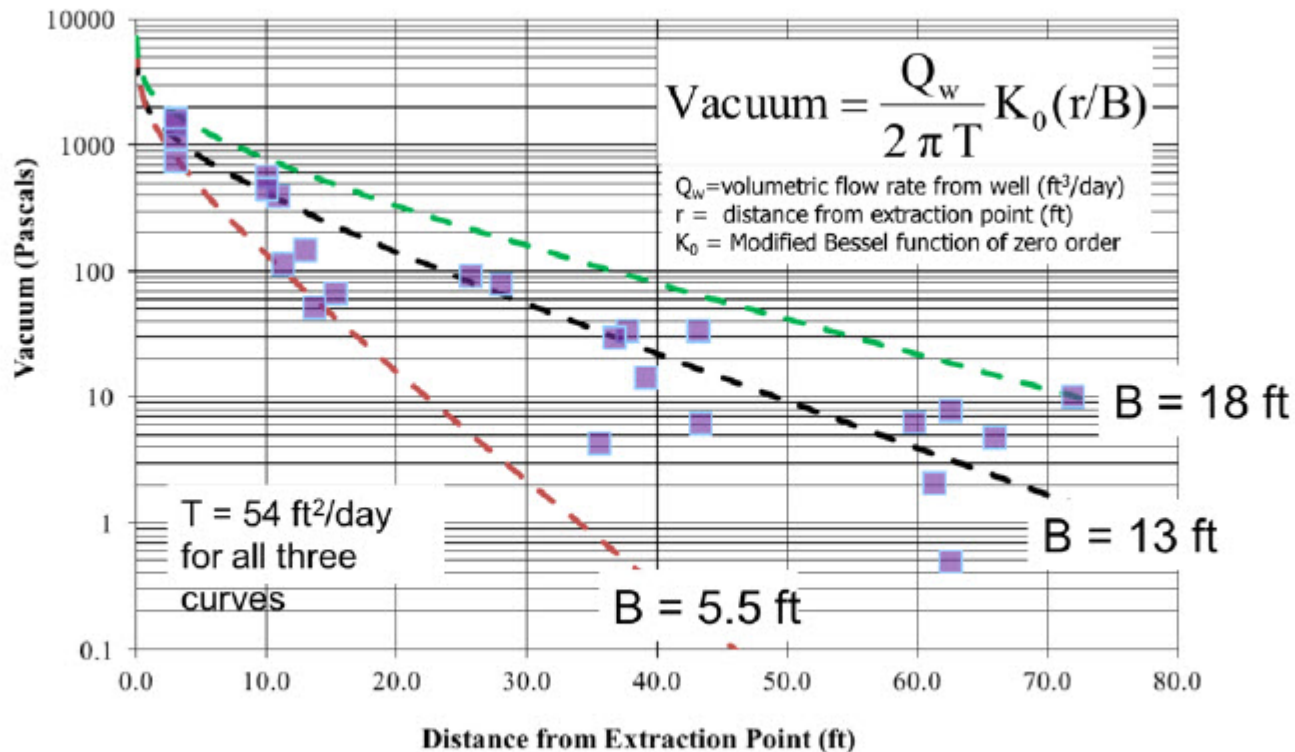
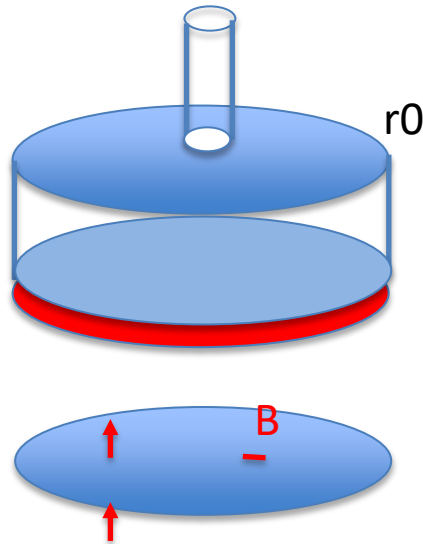


Figure (3): Comparison of vacuum vs distance measurements to profiles calculated using the Hantush-Jacob Model

Best Model For New Construction Plenum



Concrete:
 B' = thickness
 K' = Bulk pneumatic conductivity
 B = Leakage through slab

Aggregate: gravel...sand:
 T : Transmissivity in extraction zone

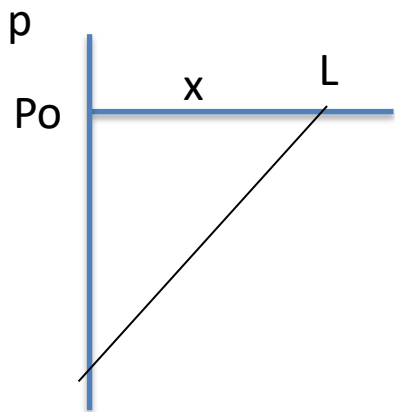
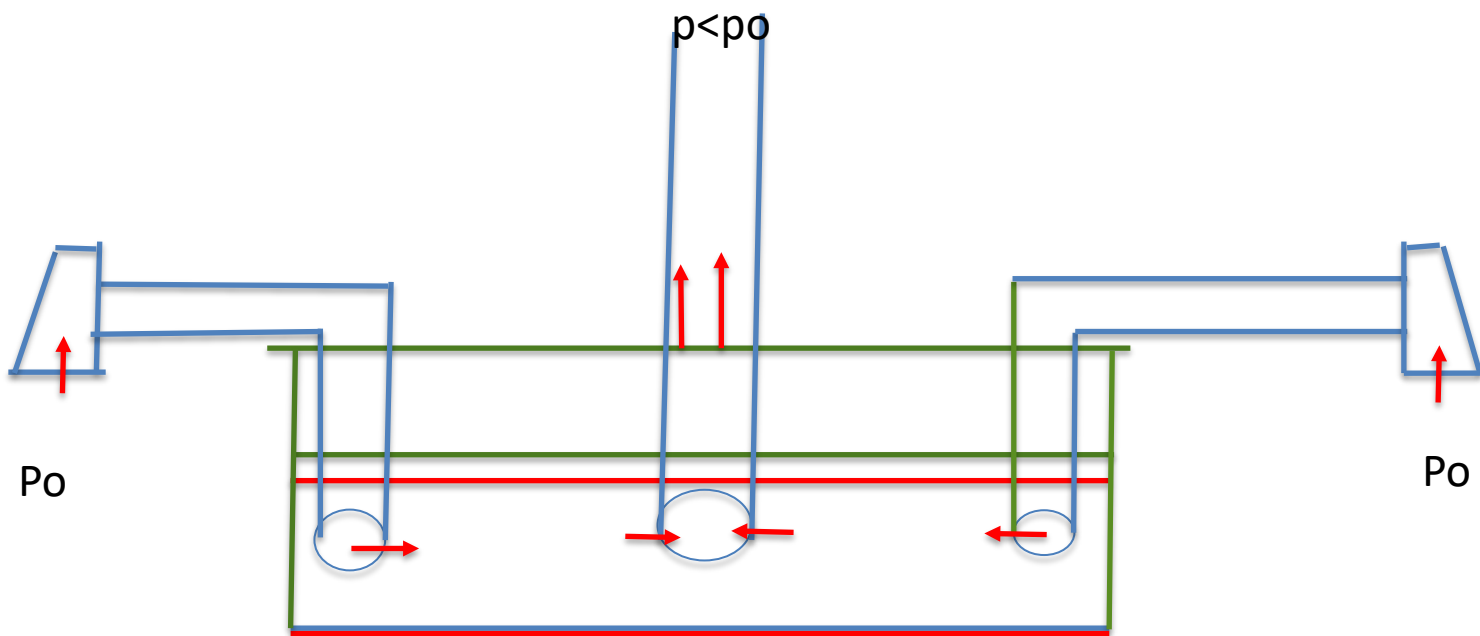
Bottom of Plenum is semipermeable with a leakage (in B)

$$P(\text{vacuum}) = Q_{ssv} / (2 \pi T) K_0(r/B)$$

$$\text{Velocity} = Q_{ssv} / (2 \pi b n B) K_1(r/B)$$

**WHAT IF IN NEW CONSTRUCTION WE COULD SIMPLY
 MAKE THE PROBLEM 1 DIMENSIONAL?**

In Line Fan imposes a vacuum



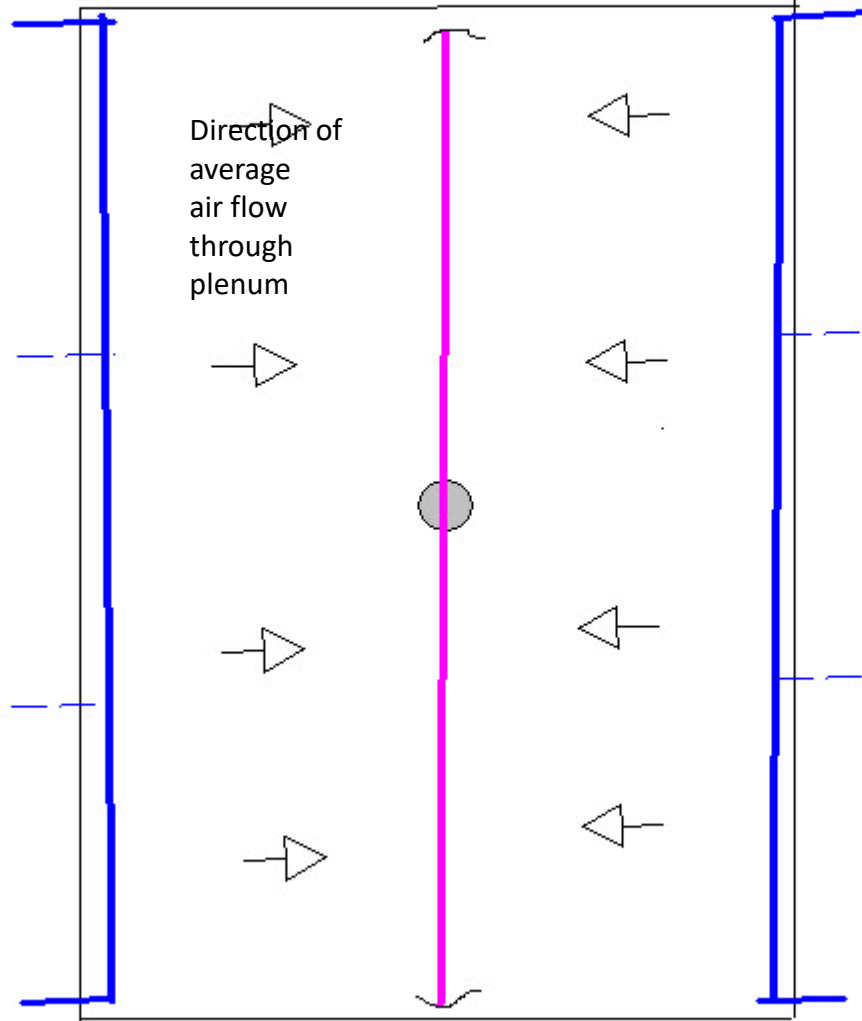
40ft x 80ft

3,200 sq.ft.

4 cfm

80 ft

Direction of
average
air flow
through
plenum



53 ft

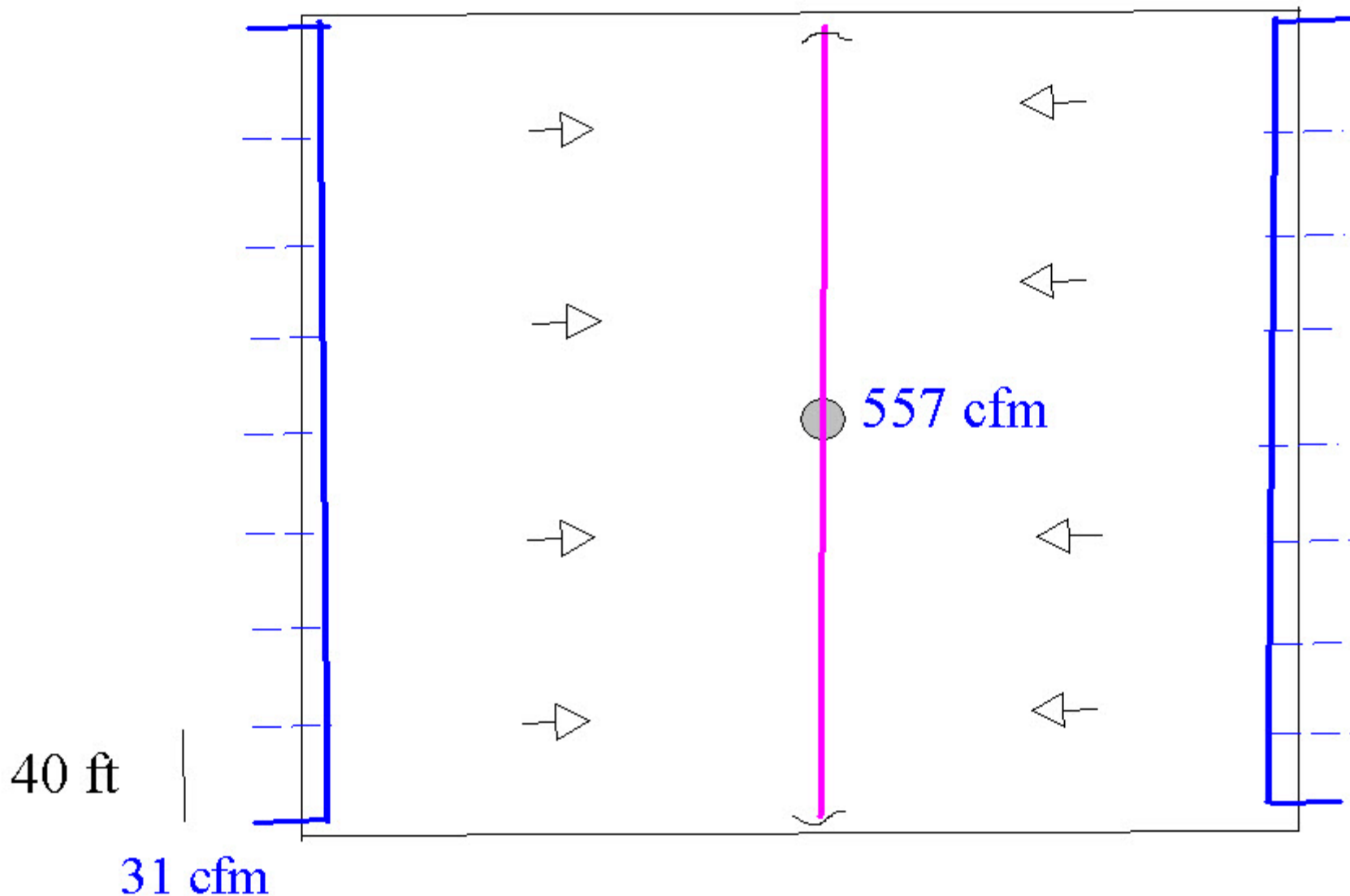
8 cfm

80ft x 160ft

317 ft x 317 ft

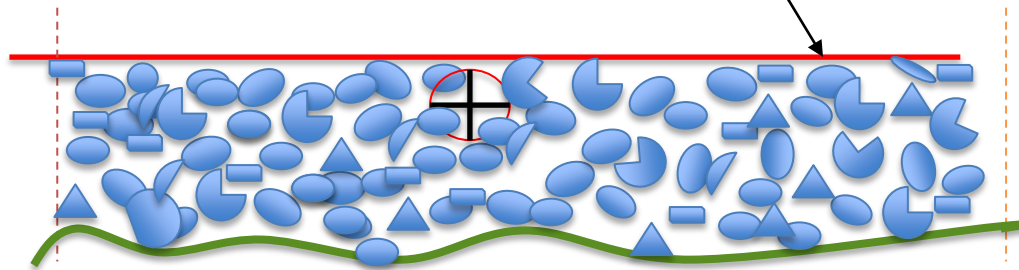
>100,000 sq. ft.

← 160 ft →



Flow model: shown is the cross section perpendicular to the direction of average air flow through the plenum

High density polyethylene sheet acting as an impenetrable barrier for air and radon (very slick plastic) Fully sealed

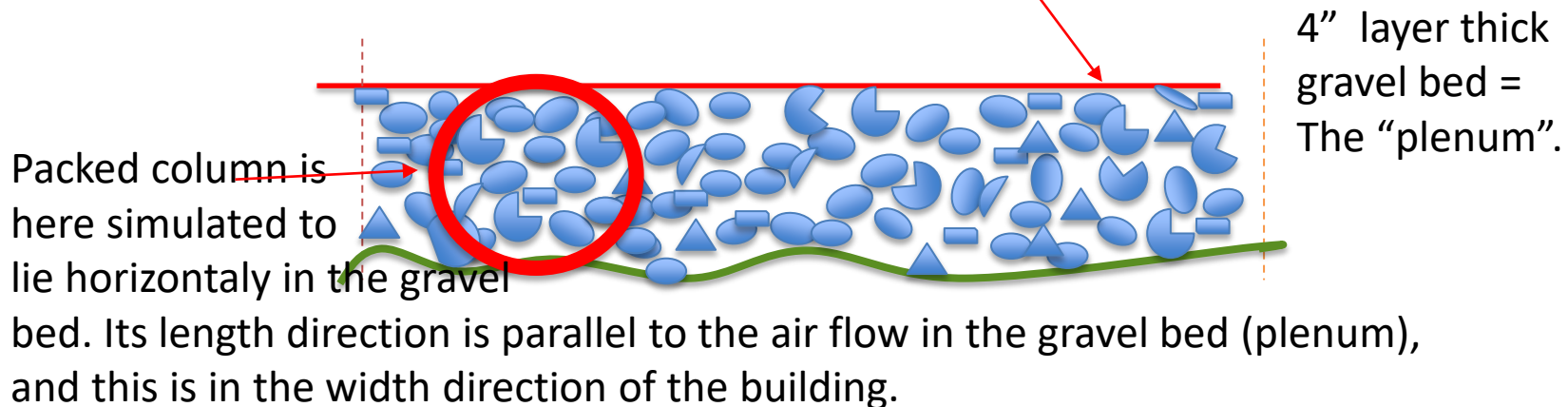


4" or 6" thick layer
The "plenum".
Reflective Boundary
Conditions on the sides,
or treat this as one cell
of many side by side.

Original soil, or compacted soil, clay, silt has a much smaller permeability for air than any other component, or best is a fully sealed sheet of high density polyethylene.

Flow model cross section perpendicular to the direction of average air flow through the plenum under the concrete slab. (The plenum is the entire gravel bed)

High density polyethylene sheet acting as an impenetrable barrier
for air and radon (very slick plastic) Fully sealed

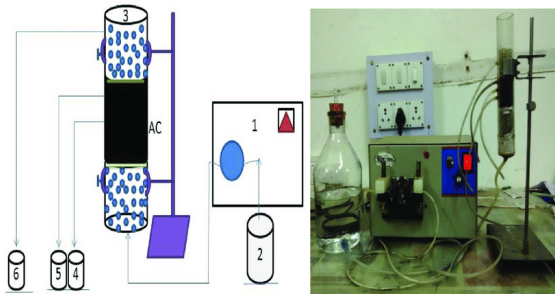


Length of the pipe inside-wall cross section (= a circle): $\pi \cdot D = 31.9$ cm
Length of equivalent cross section for the "walls of the plenum": $2 \cdot D = 20.3$ cm
Thus, the wall effects are less important in the flow under the slab than in the pipe by $1 - (2/\pi) = 36\%$

Packed columns examples



A packed column is a **pipe or hollow tube** filled with fine particles and packing materials. You can think of them as a pressure vessel with a packed section included in its final design.



1. Peristaltic pump
2. Wastewater reservoir
3. Packed column (glass beads +cotton +activated carbon +cotton +glass beads)
- 4./5./6. Sample storing vial (at each 1 cm height of filled activated carbon)



Industry: Petrochemical Distillation

Ergun Equation (1952)

Named after Sabri Ergun (Turkish Engineer)

Describes the flow through porous media.

Applicable for packed columns, 1-dimensional problem.

Used in titration, chemical reactors and adsorption columns, and packed towers, as well as the design and optimization of separation and filtration processes.

It describes the non-linear relationship between the decrease in pressure and the “superficial velocity” through the column, in the direction of the flow.

$$\bullet \Delta p = \frac{150\mu (1-\varepsilon)^2}{D_p^2 \varepsilon^3} v_s + \frac{1.75 L \rho (1-\varepsilon)}{D_p \varepsilon^3} v_s |v_s|$$

Ergun equation

Article Talk

Read Edit View history Tools

From Wikipedia, the free encyclopedia

The **Ergun equation**, derived by the [Turkish chemical engineer Sabri Ergun](#) in 1952, expresses the friction factor in a [packed column](#) as a function of the modified [Reynolds number](#).

Equation [edit]

$$f_p = \frac{150}{Gr_p} + 1.75$$

where f_p and Gr_p are defined as

$$f_p = \frac{\Delta p}{L} \frac{D_p}{\rho v_s^2} \left(\frac{\epsilon^3}{1 - \epsilon} \right) \quad \text{friction factor}$$

and

$$Gr_p = \frac{\rho v_s D_p}{(1 - \epsilon)\mu} = \frac{Re}{(1 - \epsilon)}$$

$$y = \frac{150}{x} + 1.75$$

where:

Gr_p is the modified Reynolds number,

f_p is the packed bed [friction factor](#)

Δp is the [pressure drop](#) across the bed,

L is the length of the bed (not the column),

D_p is the equivalent spherical diameter of the packing,

ρ is the [density of fluid](#),

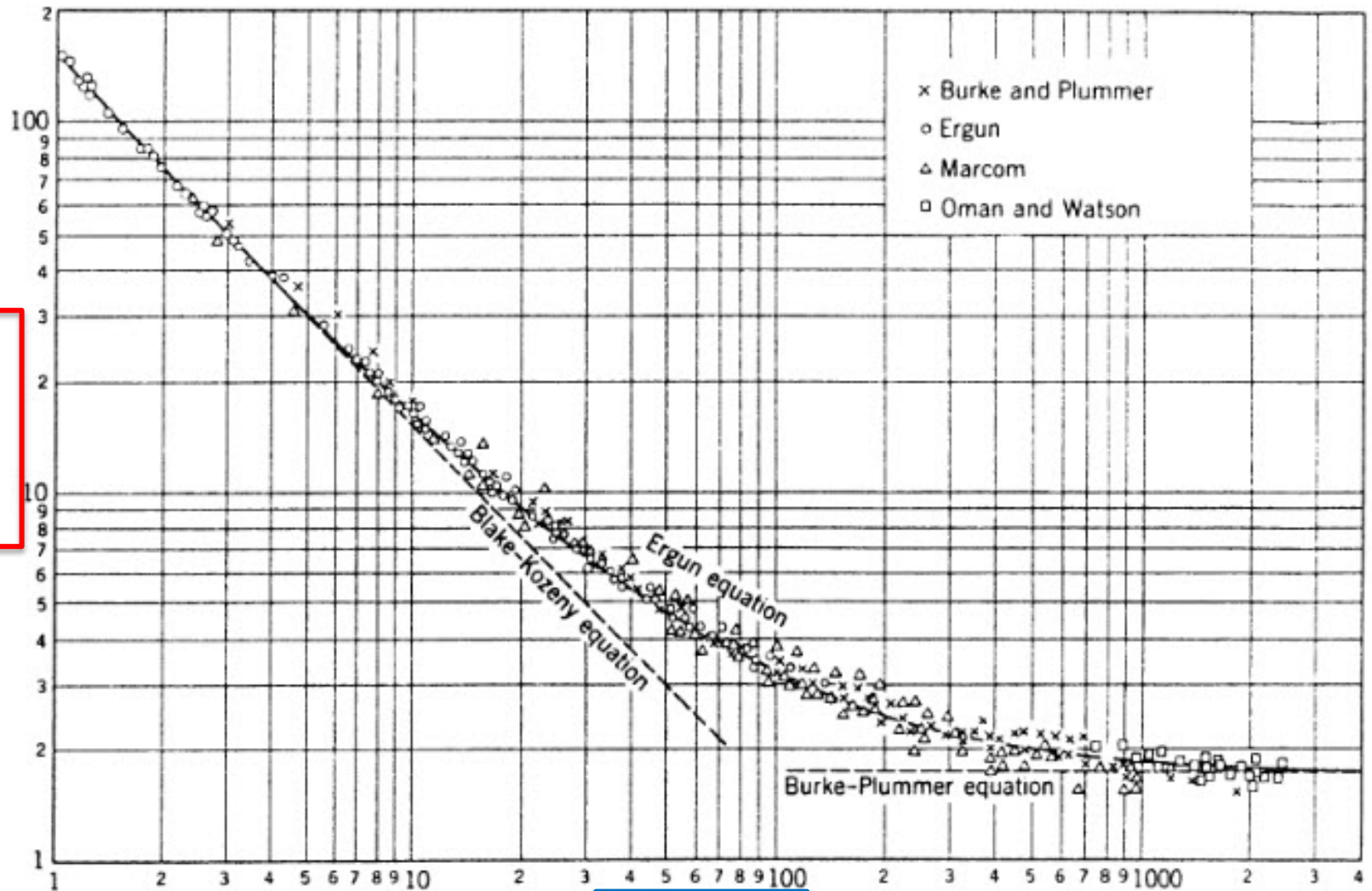
μ is the [dynamic viscosity](#) of the fluid,

v_s is the [superficial velocity](#) (i.e. the velocity that the fluid would have through the empty tube at the same volumetric flow rate)

ϵ is the void fraction ([porosity](#)) of the bed.

Re is the particle [Reynolds Number](#) (based on [superficial velocity](#)^[1]).

$$\frac{\Delta p \bar{\rho}}{G_0^2} \cdot \frac{D_p}{L} \cdot \frac{\epsilon^3}{1-\epsilon}$$



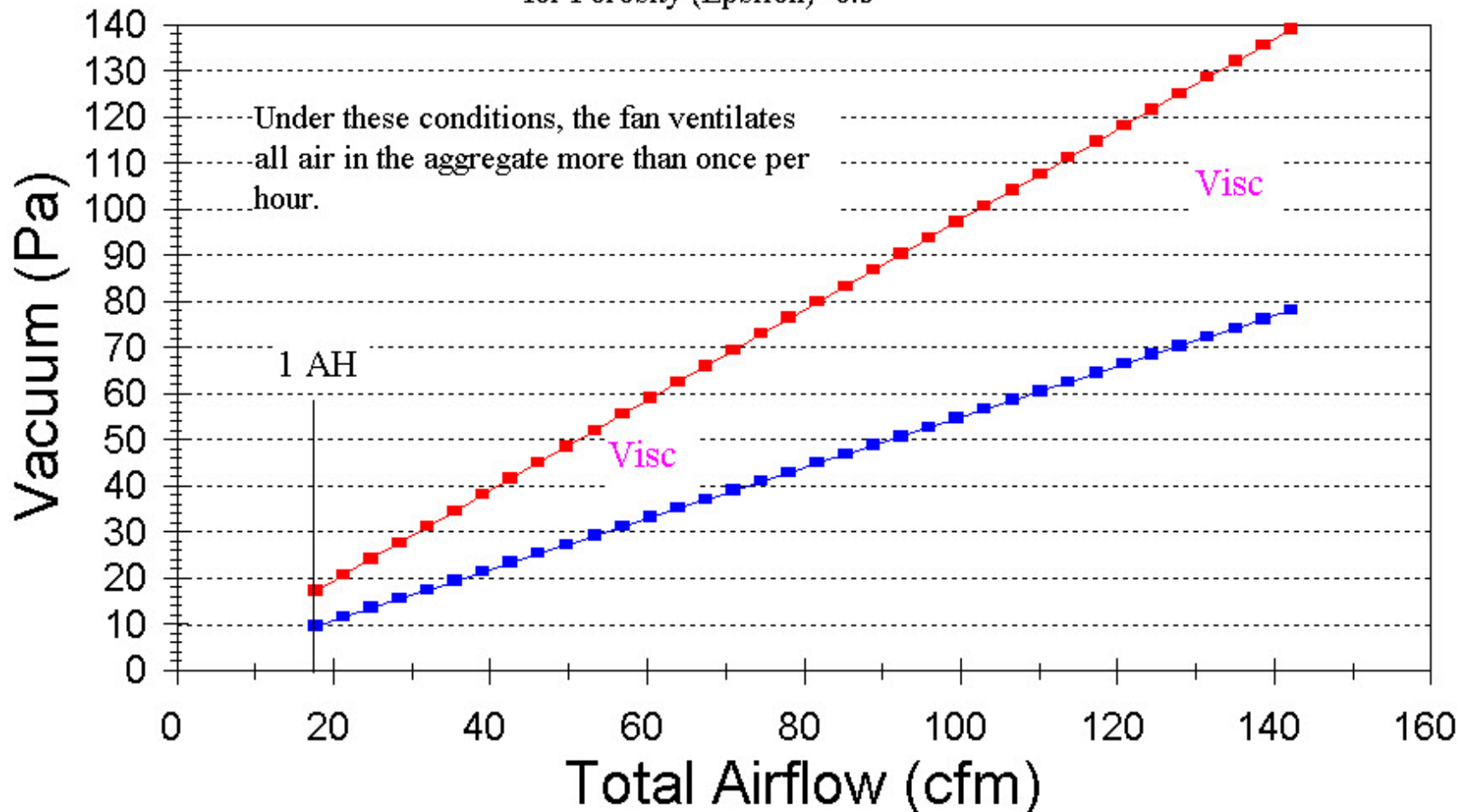
$$\frac{D_p G_0}{\mu} \cdot \frac{1}{1-\epsilon}$$

Normalised plot of the Ergun equation (after Ergun, 1952; Bird et al., 1960).

Distributed Optimized SSVentilation

SteadyState for #8 gravel (depth=4in)

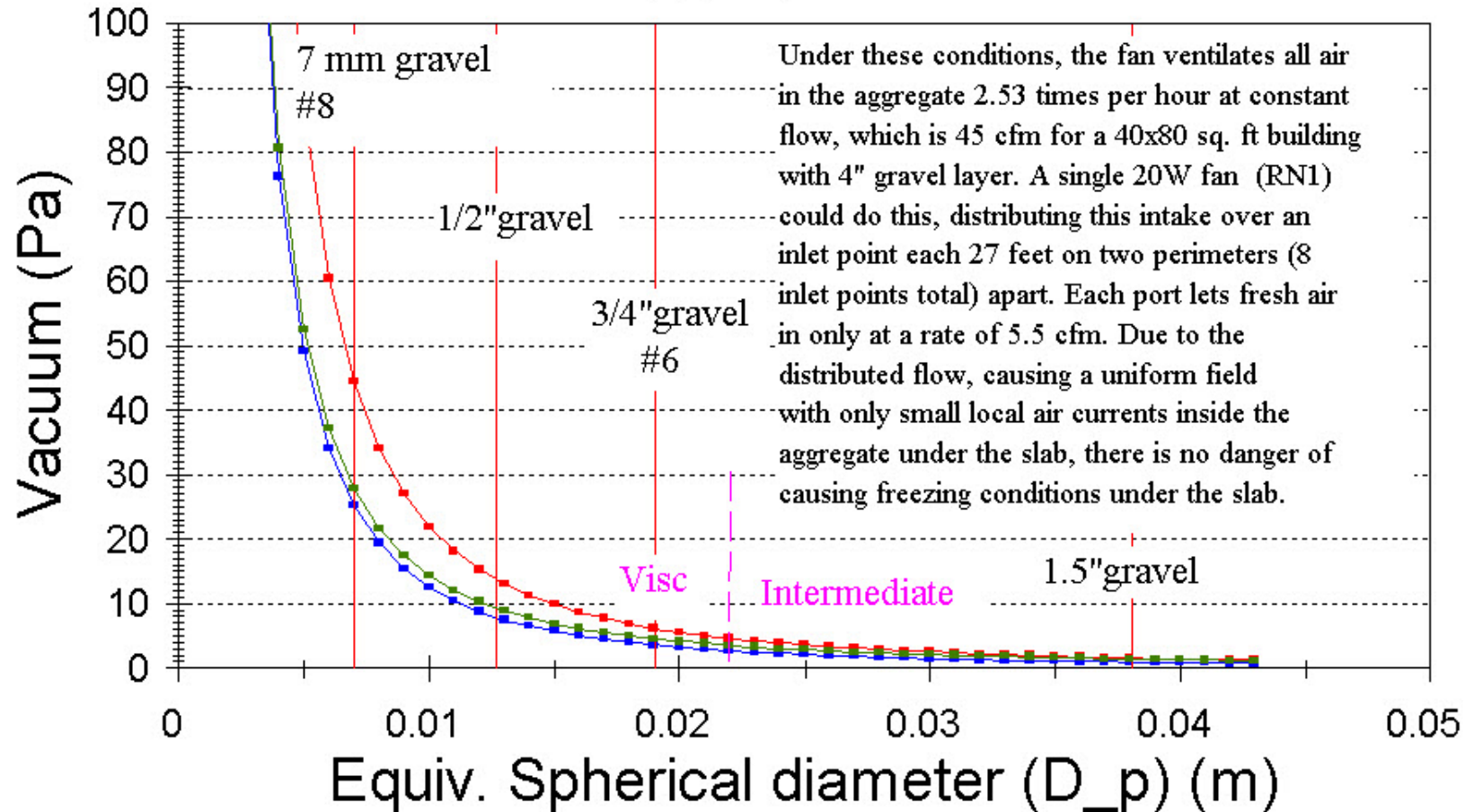
for Porosity (Epsilon)=0.3



■ Ergun 80x40=3,200 sq.ft. ■ Quinn

Distributed Optimized SSVentilation

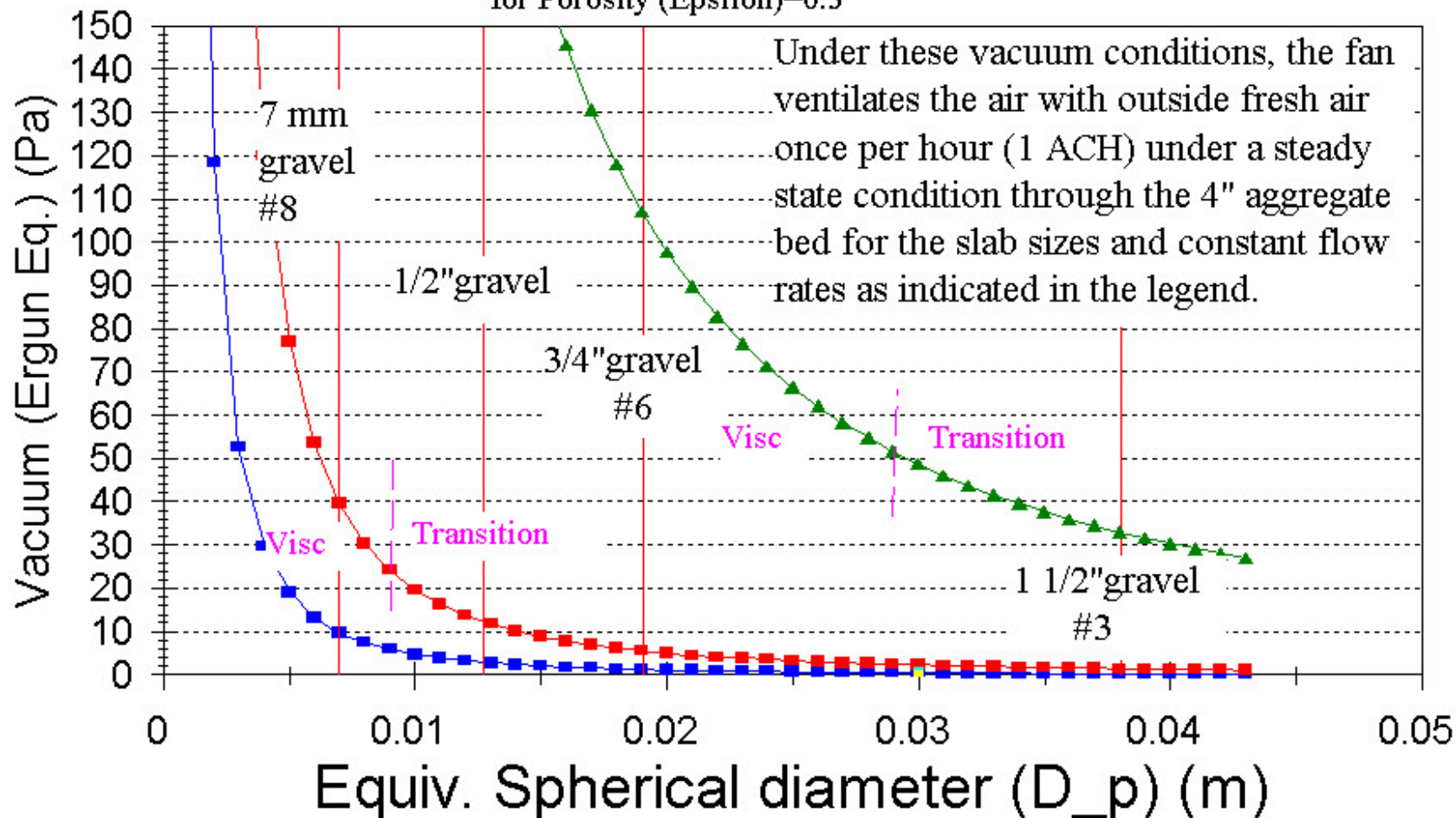
Steady State at 2.53 AH: 4" aggregate
for Porosity (Epsilon)=0.3



- Ergun for 80x40=3200 sq.ft. 45 cfm
- Lieu
- Quinn

Distributed Optimized SSVentilation

SteadyState at 1ACH with 4inch aggregate.
for Porosity (Epsilon)=0.3



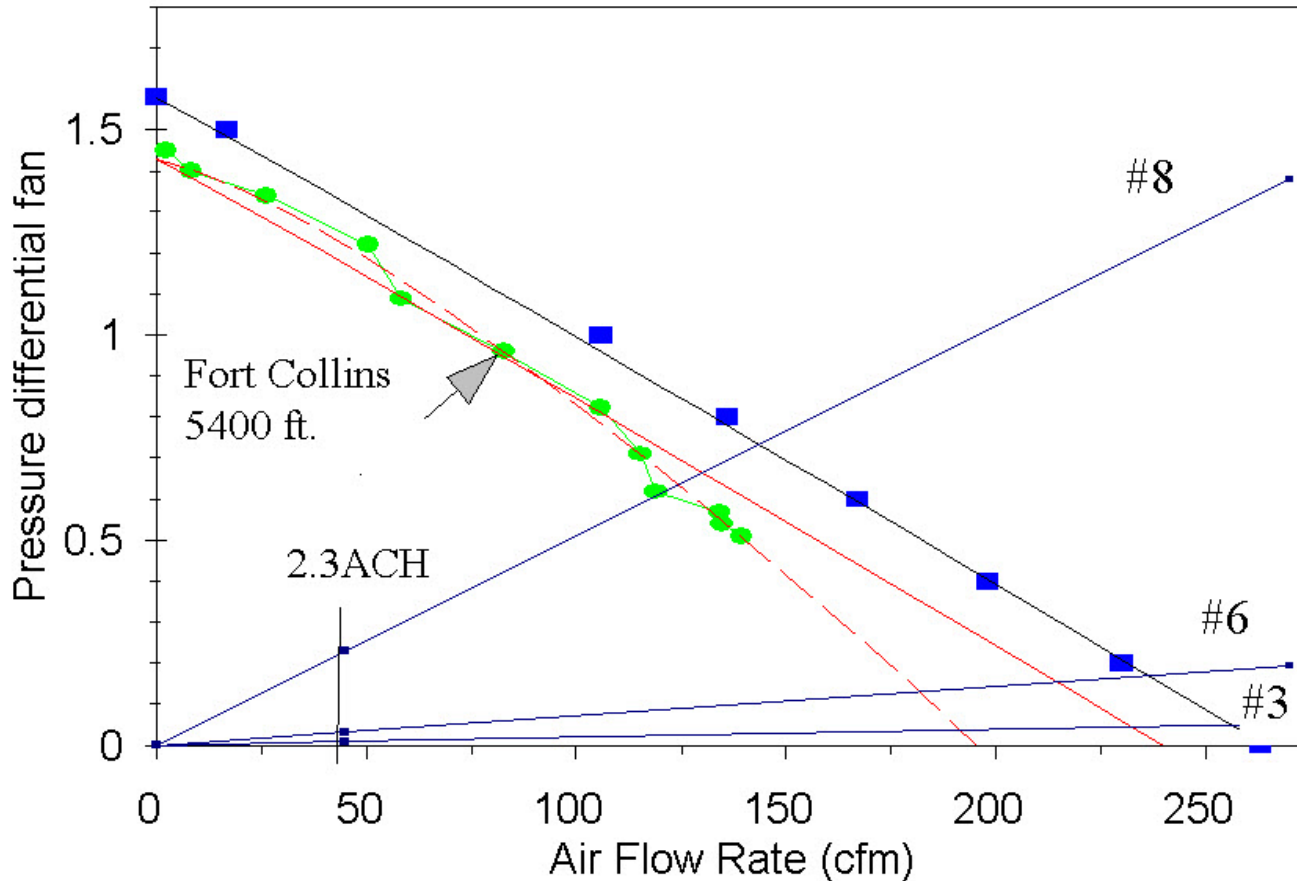
■ 17.8 cfm for 80x40=3,200sq.ft.

■ 71.1 cfm for 160x80=12,800sq.ft.

▲ 558.2 cfm for 317x317=100,489 sq.ft.

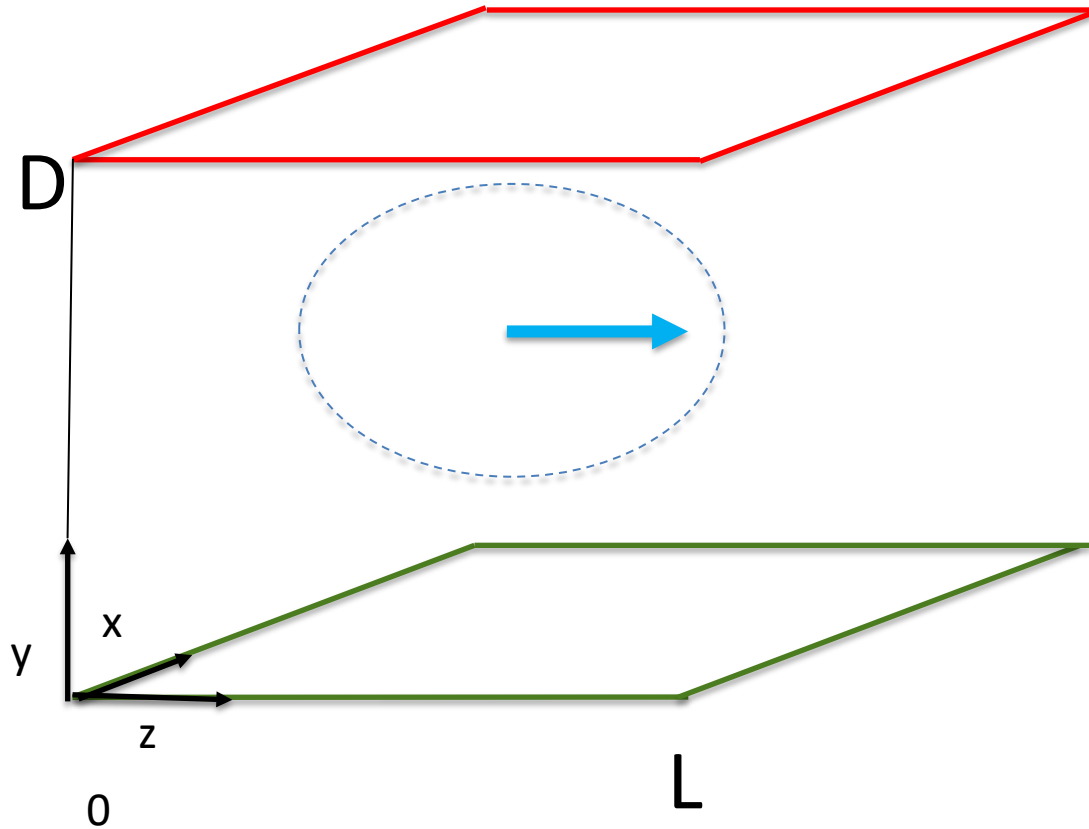
Fan Response Curve

FR150 Max "7"

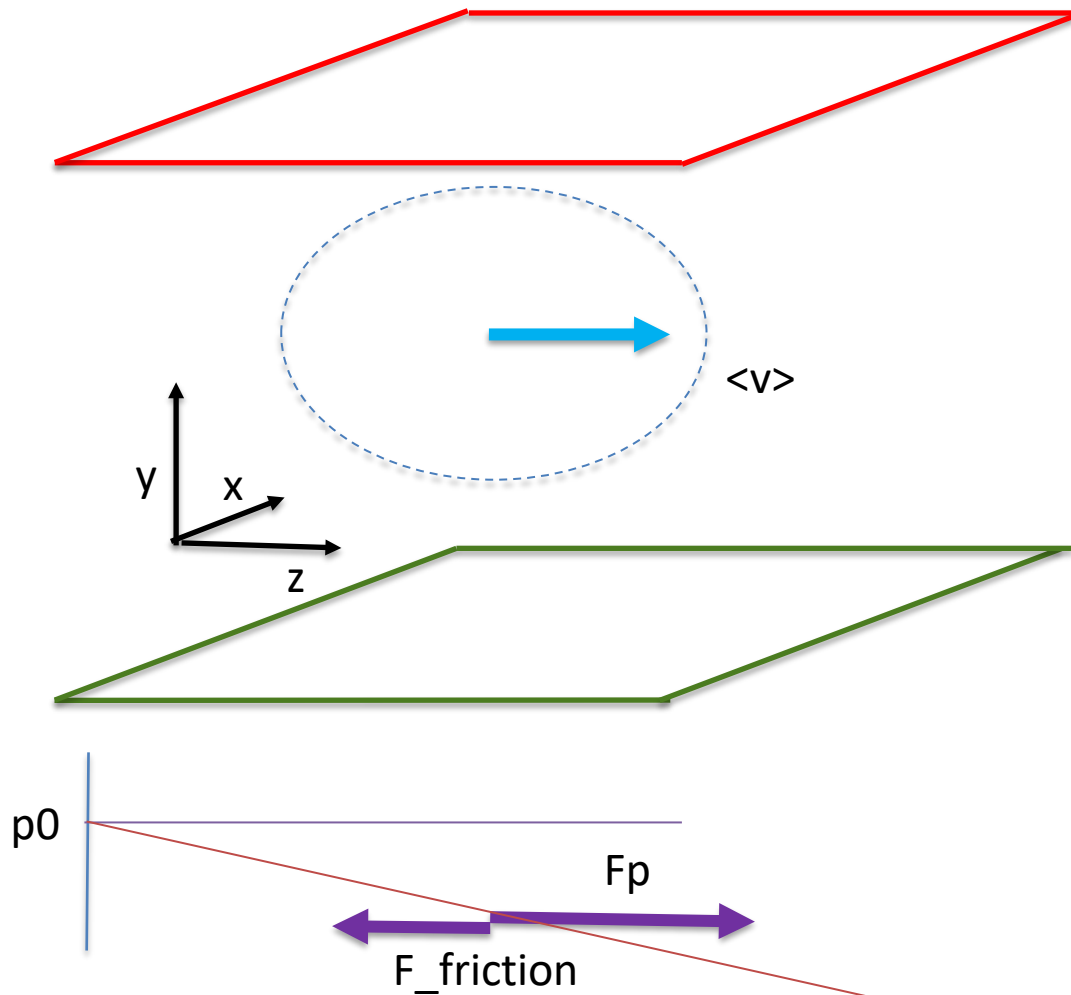


Current medium power fans have much more power than are needed for DOSSV flow rate

The Physical Model



Consider a mesoscopic unit control volume (element) (fluid, or air) and describe parameters averaged per unit of volume (density, instead of mass).



A net force will accelerate an object: 2nd law of motion (Newton)

$$F = m \, dv/dt$$

If no net force acts on an object, it will maintain its motion: 1st Law of Newton

Second law of Motion (Newton):

$$m \frac{d\vec{u}}{dt} = \vec{F} \quad F(\text{gravity})$$

Fluid dynamics model (Navier Stokes Eq.):

$$\rho \frac{d\vec{u}}{dt} = -\rho g \vec{k} - \vec{\nabla} p + \mu \Delta \vec{u} + \vec{f}_{ext}$$

f(gravity) f(pressure) f(viscous) + f(friction with aggregate)

Employ symmetries of the problem,
and the Boundary Conditions (BCs)
and Initial Conditions.

Choose the z-axis to point parallel to the equilibrium velocity vector (local average of volume flow on a volume element, Darcy velocity) is given by:

$$\vec{q} = -\frac{k}{\mu} \frac{dp}{dz} \vec{e}_z$$

(In opposite direction to the increase of pressure)

RESULTS FROM EXPERIMENTS OF FLUIDS DISSIPATING THROUGH PACKED COLUMNS:

It describes the control volume is

“sliding down the hill towards lower pressures”

This is the result of a balancing act of the pressure force with the friction forces due to the air being forced to go through the many small connected holes and curved pathways (pores), taking into account the fluid's internal viscosity.

Use Energy conservation

- $p(x, y, z, t) = p_0 \left(\frac{z}{L} \right) + \text{terms dying off quickly}$
- How quickly?
- $\tau_{c1} < \frac{\alpha}{\left(\frac{\pi}{D}\right)^2} = \alpha \left(\frac{D}{\pi}\right)^2 = \left(\frac{\theta_a \mu}{k P_0}\right) \left(\frac{D}{\pi}\right)^2 \equiv \tau_{c2}$
- $\vec{f}_z = -\vec{\nabla} p_\infty(z) = -\frac{p_0}{L} \vec{e}_z$
- The pressure force on each volume element **everywhere in the aggregate** is constant, the same, and in the same direction, (homogeneous and isotropic), as is also the averaged friction forces,
-and they will balance each other out

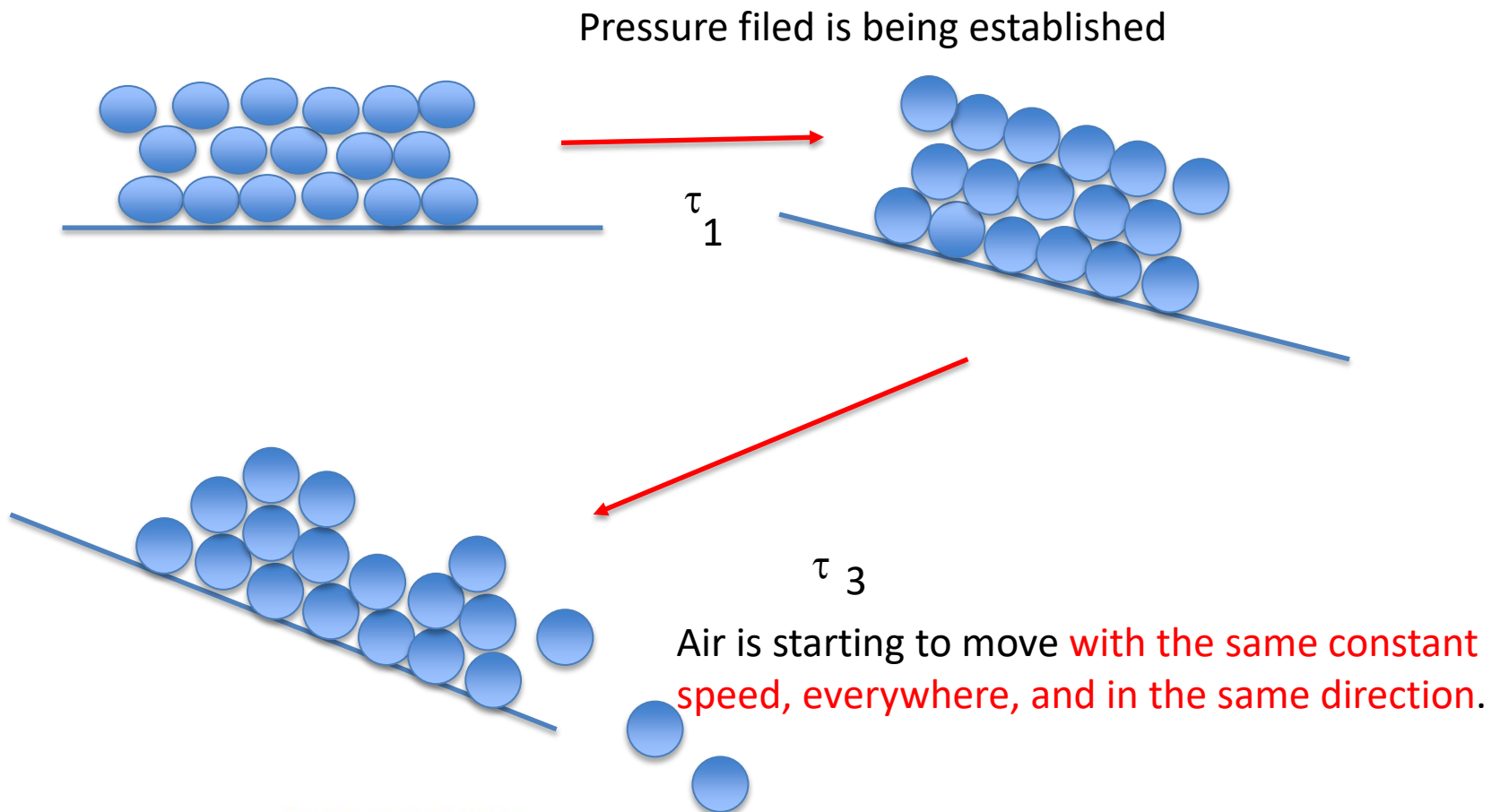
- The resulting equilibrium average speed, averaged over the volume element, is given by the Darcy equation:

- $$\vec{q} = -\frac{k}{\mu} \frac{dp}{dz} \vec{e}_z = -\frac{k}{\mu} \frac{p_0}{L} \vec{e}_z$$

which is constant and isotropic, when averaged over a volume element.

“Dumptruck” Model

(for DOSSV only, not for ASD)



Characteristic time scales

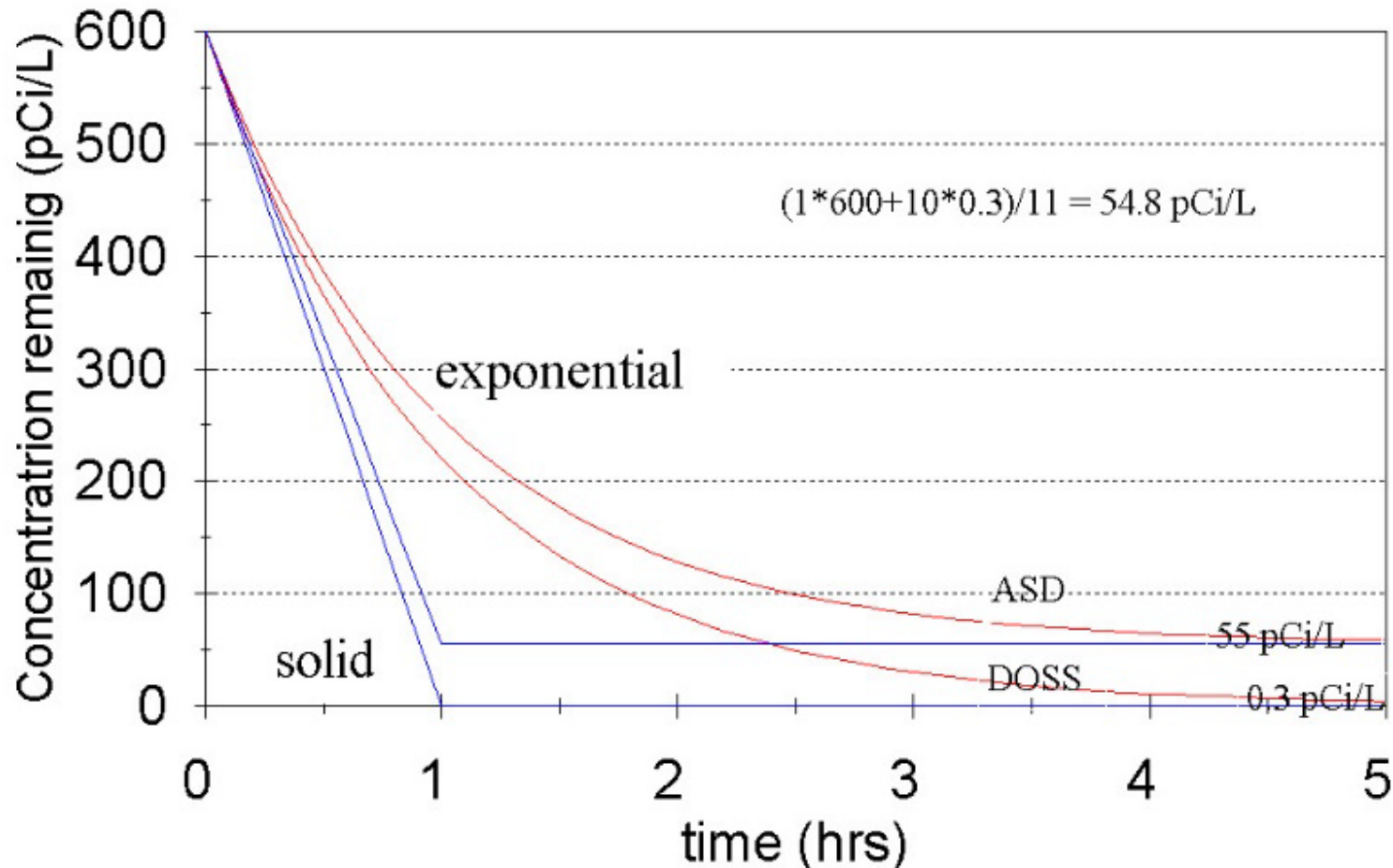
Characteristic time	Gravel	Clean sand	Silty sand
Typical intrinsic permeability (k)	10^{-9} m^2	10^{-11} m^2	10^{-12} m^2
For vertical (y) pressurization of plenum with D=4"	$5.3 \cdot 10^{-5} \text{ s}$	0.0053 s	0.053 s
For distance from supply to discharge pipes (z) (20 ft)	0.19 s	19.2 s	192 s



Efficiency for radon removal of DOSSV is better than ASD

Filtration models

Conc. under slab @1 ACH vent. rate



Summary of Radon Mitigation Models

- (1) Reddy-Sextro et al. model (EPA, 1992), 2 dim, air movement through soil under foundation walls.
Dynamics: Pressures and flows in plenum are vastly different close to pipe (turbulent), compared to far away (laminar).
- (2) Hantusch-Jacob model (T. McAlary, 2018), “Leaky aquafer”: 2- dim, leaks from above & leaks from below
Dynamics: Same comment as in (1).
- (3) New, DOSSV proposed for new construction allows solving a much simpler 1- dim problem, Air vacuum and flow through the aggregate bed (plenum) can be calculated for any gravel or sand with known characteristics.
Dynamics: flow is the same throughout the aggregate. (**homogeneous and isotropic**). (Viscous (laminar), or Transition regime)

Advantages of Using the DOSSV configuration over ASD in New Home Construction:

- **Final radon concentrations** are expected **lower** than with ASD because we replace with fresh air. (higher efficiency)
- **# of main vent pipes** in large footprint buildings, or large open work areas **can be reduced**, due to the higher radon removal efficiency.
- **Lower power radon fans** can be as effective as ASD for equivalent sized buildings.
- Design can be **optimized during architectural phase**, and for a less optimal situation, the resulting pressure and flow can still be calculated based on the info of gravel used, or chosen.
- The same configuration **can be used to minimize Vapor Intrusion** more effectively into the building.